

# Perturbation-Admissible Structural Stability in the UNNS Substrate

Admissibility Geometry, Phase Boundaries, and Quotient Descent in  
Co-Seismic Rank and Topology Invariance

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## Abstract

Within the UNNS Substrate framework, every co-seismic displacement hierarchy is a realization inside an admissible operator family, and structural stability is the statement that the induced signature descends through the quotient by admissible transforms. We formalize this descent condition as perturbation-admissible structural stability, instantiated concretely on the LXV seismic chamber suite. Smoothing windows  $w \in W$  act as nested resolution morphisms on the substrate; the perturbation envelope  $\|\mathbf{u}_w - \mathbf{u}_1\| \leq \sigma_P$  is bounded admissible deformation within the operator grammar. We introduce two rigidity moduli – the magnitude modulus  $\mathcal{R}_{\text{mag}} = \min_k \Delta_k / (2\sigma_P)$  and the geometric modulus  $\mathcal{R}_{\text{geo}} = \Theta_{\text{min}} / (2\delta_P)$  – whose joint value  $\mathcal{R} = (\mathcal{R}_{\text{mag}}, \mathcal{R}_{\text{geo}})$  constitutes the admissibility margin of the event. We prove that  $\mathcal{R} > (1, 1)$  is sufficient for full descent (Order Rigidity and Directional Stability), derive tight inversion bounds via the matching number  $\nu(V)$  of vulnerable gaps, and establish a Phase-Boundary Theorem showing that boundary degeneracy is structurally forced whenever either modulus reaches 1. Three earthquake events spanning two orders of magnitude in  $\mathcal{R}_{\text{mag}}$  confirm the predicted phase structure and demonstrate that the admissibility margin encodes near-fault geometry independently of event magnitude.

## 1 Preliminaries

Let  $\mathcal{N}$  be a finite station set with  $|\mathcal{N}| = N$ .

Let  $S_w(i)$  denote the co-seismic horizontal displacement magnitude computed under smoothing window  $w$ .

Let  $R_w$  denote the total order induced by  $S_w$ .

Let  $w_0 = 1$  denote the baseline window throughout.

**Definition 1** (Inversion Distance). *For window  $w$ , define*

$$D(w) = \#\{(i, j) : R_{w_0}(i) < R_{w_0}(j) \text{ but } R_w(i) > R_w(j)\}.$$

**Definition 2** (Perturbation-Admissible Family). *A smoothing family  $\mathcal{W}$  is perturbation-admissible if:*

1. (Symmetry) *All windows are symmetric and centered. Used in: the sub-Gaussian proxy bound of Lemma 1, where centered averaging implies the smoothed noise has zero mean.*
2. (Guard consistency) *Guard convention is fixed across all windows. Used in: the epoch count  $m$  is the same for every  $w$ , so the envelope  $\sigma_P(\alpha)$  is computed uniformly.*
3. (Detrending invariance) *Detrending protocol is invariant. Used in: the residual model of Definition 7, which assumes post-detrending mean-zero noise.*
4. (Finiteness) *Window size is finite. Used in: all probability bounds require finitely many samples  $m < \infty$ .*

## 2 Rigid–Nonrigid Transition Principle (RNP)

**Principle 1** (Rigid–Nonrigid Transition). *Let  $\mathcal{O}$  be an induced order under a perturbation operator  $P_\epsilon$ . There exists a critical perturbation scale  $\epsilon_c$  such that:*

$$\begin{aligned} \epsilon < \epsilon_c &\implies \mathcal{O} \text{ rigid} \\ \epsilon \geq \epsilon_c &\implies \mathcal{O} \text{ admits degeneracy} \end{aligned}$$

**Seismic instantiation.** In the co-seismic ranking context the RNP critical scale is instantiated as

$$\epsilon_c = \frac{1}{2} \min_k \Delta_k,$$

the half-width of the smallest adjacent gap. The perturbation amplitude is  $\sigma_P$  (see Definition 4 and 5). The Rigidity Modulus  $\mathcal{R} = \epsilon_c/\sigma_P$  therefore measures the distance from the transition boundary:  $\mathcal{R} > 1$  is exactly the RNP condition  $\sigma_P < \epsilon_c$ , while  $\mathcal{R} \leq 1$  places the system at or below the transition threshold.

### 3 Rigidity Modulus

**Definition 3** (Adjacent Gap). *For baseline ranking  $R_{w_0}$  with magnitudes*

$$S_{w_0}(i_1) \geq S_{w_0}(i_2) \geq \dots \geq S_{w_0}(i_N),$$

*define adjacent gaps:*

$$\Delta_k = S_{w_0}(i_k) - S_{w_0}(i_{k+1}).$$

The Rigidity Modulus depends on how  $\sigma_P$  is estimated. We distinguish three notions that share intuition but differ operationally; all are defined relative to the same canonical form  $\mathcal{R} = \min_k \Delta_k / (2\sigma_P)$ .

**Definition 4** (Empirical Perturbation Amplitude). *The empirical perturbation amplitude is the worst-case observed deviation:*

$$\sigma_P^{(\text{emp})} := \max_{s \in \mathcal{N}, w \in W \setminus \{w_0\}} |S_w(s) - S_{w_0}(s)|.$$

**Definition 5** (Probabilistic Perturbation Envelope). *For confidence level  $\alpha \in (0, 1)$ , the probabilistic perturbation envelope is*

$$\sigma_P(\alpha) := \max_{w \in W} \left( 2c_{\text{med}} \sigma \sqrt{1 + \frac{1}{w} \sqrt{\frac{\log(4/\alpha)}{m}}} \right),$$

*where  $\sigma$  is the sub-Gaussian noise proxy (Section 5),  $m$  is the number of usable epochs (Definition 7), and  $c_{\text{med}}$  is a universal constant bounded in Remark 2.*

**Remark 1** (Relationship between the two amplitudes). *By Theorem 2,  $\sigma_P^{(\text{emp})} \leq \sigma_P(\alpha)$  with probability at least  $1 - \alpha$ . Hence the empirical Rigidity Modulus*

$$\widehat{\mathcal{R}}(\alpha) := \frac{\min_k \Delta_k}{2\sigma_P(\alpha)}$$

*is a data-specific lower bound on the true modulus: if  $\widehat{\mathcal{R}}(\alpha) > 1$  then the rank is rigid with probability at least  $1 - \alpha$ .*

**Definition 6** (Rigidity Modulus – Canonical Form). *For either amplitude variant:*

$$\mathcal{R} := \frac{\min_k \Delta_k}{2\sigma_P}.$$

**Running example.** For LXV-B2 (El Mayor 2010), baseline magnitudes are 104.94, 49.11, 7.95, 7.46, 6.96 mm, giving  $\min \Delta_k = 0.484$  mm. Empirically  $\sigma_P^{(\text{emp})} \approx 1.3$  mm, so  $\mathcal{R} = 0.484/(2 \times 1.3) \approx 0.19$ . Vulnerable gaps:  $|V| = 2$  (the two sub-millimetre tail gaps). Degeneracy Bound:  $D(w) \leq |V|(N-1) = 2 \times 4 = 8$ . Observed  $D = 1$  in selected windows – consistent with boundary degeneracy. This worked example is revisited at each theoretical step below.

## 4 Deterministic Order Rigidity

**Theorem 1** (Order Rigidity). *If  $\mathcal{R} > 1$  (equivalently,  $\min_k \Delta_k > 2\sigma_P$ ), then*

$$D(w) = 0 \quad \forall w \in \mathcal{W}.$$

*Contradiction outline.* Assume  $\mathcal{R} > 1$  but  $D(w) > 0$  for some  $w$ . Then there exists an adjacent pair  $(i_k, i_{k+1})$  such that  $S_w(i_k) < S_w(i_{k+1})$ . By the perturbation bound each station’s displacement changes by at most  $\sigma_P$  (Admissibility condition 1), so

$$S_w(i_k) \geq S_{w_0}(i_k) - \sigma_P, \quad S_w(i_{k+1}) \leq S_{w_0}(i_{k+1}) + \sigma_P.$$

Inversion requires  $S_w(i_{k+1}) - S_w(i_k) > 0$ , hence  $\Delta_k = S_{w_0}(i_k) - S_{w_0}(i_{k+1}) \leq 2\sigma_P$ , contradicting  $\mathcal{R} > 1$ .  $\square$

**Running example (continued).** LXV-B2 has  $\mathcal{R} \approx 0.19 < 1$ , so Theorem 1 does *not* apply; inversions are permitted. LXV-A (Kumamoto) has  $\mathcal{R} \approx 21.6 \gg 1$ , so the theorem guarantees  $D(w) = 0$  for every window – as observed.

## 5 Probabilistic Quantitative Rigidity

Theorem 1 is the worst-case (deterministic) result. We now derive a stronger probabilistic version that makes  $\mathcal{R}$  computable from noise observations.

### 5.1 Assumptions

**Definition 7** (Residual Noise Model). *After the LXV pre-fit detrending step, suppose each component residual  $\varepsilon_s(t)$  (for each station  $s$ ) is conditionally mean-zero and  $\sigma$ -sub-Gaussian:*

$$\mathbb{E}[\exp(\lambda \varepsilon_s(t))] \leq \exp\left(\frac{\lambda^2 \sigma^2}{2}\right) \quad \forall \lambda \in \mathbb{R}.$$

We assume independence across epochs within each side-window (pre vs. post) for bounding purposes. Let  $m_{\text{pre}}$  and  $m_{\text{post}}$  be the number of usable epochs in each side after guard and coverage gates; set  $m := \min(m_{\text{pre}}, m_{\text{post}})$ .

## 5.2 Centered Moving-Average Smoothing Bound

Let  $\text{MA}_w$  denote centered moving average of odd window length  $w$ . For i.i.d. mean-zero  $\sigma$ -sub-Gaussian noise, the smoothed residual  $\tilde{\varepsilon}^{(w)}(t) := (\text{MA}_w \varepsilon)(t)$  is sub-Gaussian with proxy  $\sigma_w \leq \sigma/\sqrt{w}$  (Admissibility condition 1 is used here). Consequently, the difference between baseline and smoothed noise satisfies

$$\varepsilon(t) - \tilde{\varepsilon}^{(w)}(t) \text{ is sub-Gaussian with proxy } \sigma_{\Delta}(w) \leq \sigma \sqrt{1 + \frac{1}{w}}.$$

## 5.3 Median-of-Window Perturbation Bound

LXV step extraction uses guarded window summaries on the pre and post sides. Let  $\text{Med}_m(\cdot)$  denote the sample median of  $m$  independent samples.

**Lemma 1** (Median Concentration). *There exists a universal constant  $c_{\text{med}} > 0$  such that for any  $\alpha \in (0, 1)$ ,*

$$\Pr\left(|\text{Med}_m(X) - \text{Med}(X)| \geq c_{\text{med}} \sigma_X \sqrt{\frac{\log(2/\alpha)}{m}}\right) \leq \alpha,$$

whenever  $X$  is  $\sigma_X$ -sub-Gaussian.

**Remark 2** (Bound on  $c_{\text{med}}$ ). *For Gaussian noise, standard order statistics give  $c_{\text{med}} = \sqrt{\pi/2} \approx 1.253$ . A conservative choice valid for any sub-Gaussian distribution is  $c_{\text{med}} = 2$ , which is sufficient for all empirical computations in Section 12.*

**Theorem 2** (Explicit Smoothing Envelope for Step Estimates). *Fix  $\alpha \in (0, 1)$  and  $w \in W$ . With probability at least  $1 - \alpha$ ,*

$$\left|\hat{\Delta}_s(w) - \hat{\Delta}_s(1)\right| \leq 2c_{\text{med}} \sigma \sqrt{1 + \frac{1}{w}} \sqrt{\frac{\log(4/\alpha)}{m}} \leq \sigma_P(\alpha).$$

## 5.4 Probabilistic Rigidity

**Theorem 3** (Quantitative Order Rigidity). *If  $\hat{\mathcal{R}}(\alpha) > 1$  then with probability at least  $1 - \alpha$ ,*

$$D(w) = 0 \quad \forall w \in W.$$

*Proof sketch.* If  $\widehat{\mathcal{R}}(\alpha) > 1$ , then  $\min_k \Delta_k > 2\sigma_P(\alpha)$ . By Theorem 2, with probability at least  $1 - \alpha$  every station deviation satisfies  $|S_w(s) - S_1(s)| \leq \sigma_P(\alpha)$ . Applying the deterministic argument of Theorem 1 with  $\sigma_P = \sigma_P(\alpha)$  completes the proof.  $\square$

Note that Theorem 1 is the limiting case  $\alpha \rightarrow 0$  (worst-case envelope) of Theorem 3: the deterministic result is the boundary of the probabilistic family.

## 5.5 Operational estimation of $\sigma$

The parameter  $\sigma$  is estimable from detrended residuals. A robust estimator is the scaled median absolute deviation:

$$\widehat{\sigma} := 1.4826 \cdot \text{MAD}(\varepsilon_s(t)).$$

This yields an empirical  $\widehat{\sigma}_P(\alpha)$  and therefore an empirical  $\widehat{\mathcal{R}}(\alpha)$ .

**Remark 3** (SNR gate as a noise-model check). *The LXV chambers gate each station on  $\text{SNR}_h \geq 5$ , where*

$$\text{SNR}_h = \frac{S_1(s)}{1.4826 \cdot \text{MAD}(\varepsilon_s(t))} = \frac{S_1(s)}{\widehat{\sigma}_s}.$$

*This is exactly the condition  $S_1(s) \geq 5\widehat{\sigma}_s$ : the baseline signal must exceed five noise standard deviations. Stations failing this gate have unreliable  $\Delta_k$  estimates and are excluded before computing  $\mathcal{R}$ .*

## 6 Boundary Regime and Degeneracy Index

**Definition 8** (Degenerate Boundary). *If  $0 < \mathcal{R} \leq 1$ , bounded inversion may occur. Define the vulnerable gap set*

$$V = \{k \in \{1, \dots, N-1\} : \Delta_k \leq 2\sigma_P\}.$$

*and the Degeneracy Index*

$$\mathcal{D} = \frac{|V|}{N-1}.$$

**Theorem 4** (General Degeneracy Bound). *Fix  $w_0 = 1$  and let baseline magnitudes be ordered  $S_1(i_1) \geq \dots \geq S_1(i_N)$  with adjacent gaps  $\Delta_k$ . Assume*

a uniform perturbation envelope  $\sigma_P$  such that  $|S_w(s) - S_1(s)| \leq \sigma_P$  for every  $s \in \mathcal{N}$ ,  $w \in W$ . Then for every  $w \in W$ :

$$D(w) \leq \sum_{k \in V} (N - k) \leq |V|(N - 1).$$

In particular, if  $V = \emptyset$  (equivalently  $\mathcal{R} > 1$ ) then  $D(w) = 0$  for all  $w \in W$ .

*Proof sketch.* Every inverted pair  $(i_a, i_b)$  with  $a < b$  can be charged to a vulnerable adjacent gap in  $V$  lying between positions  $a$  and  $b$ : by the envelope bound applied twice,  $\sum_{k=m}^{b-1} \Delta_k \leq 2\sigma_P$ , so some  $k \in V$  must exist in that block. Counting all pairs that can be charged to a given  $k \in V$  yields at most  $N - k$  choices for the upper index, giving the sum  $\sum_{k \in V} (N - k)$ . The crude bound  $N - k \leq N - 1$  produces the second inequality.  $\square$

**Theorem 5** (Degeneracy Bound – Adjacent-Swap Regime). *Under the same hypotheses as Theorem 4, assume additionally the adjacent-swap regime:*

$$\max_{s \in \mathcal{N}} |r_w(s) - r_1(s)| \leq 1,$$

*i.e. no station shifts by more than one rank relative to baseline. Then for every  $w \in W$ ,*

$$D(w) \leq |V|.$$

*Proof sketch.* Under  $\max_s |r_w(s) - r_1(s)| \leq 1$ , every inversion must be an adjacent swap across some boundary between positions  $k$  and  $k + 1$  in the baseline ordering. Such a swap can occur only if  $\Delta_k \leq 2\sigma_P$ , hence it must be charged to some  $k \in V$ . Under  $\max_s |r_w(s) - r_1(s)| \leq 1$ , crossing boundary  $k$  can only occur via the single adjacent transposition of  $(i_k, i_{k+1})$ ; any additional inversion involving that boundary would force at least one element to shift by two ranks, violating the regime assumption. Therefore distinct inversions correspond to distinct elements of  $V$ , giving  $D(w) \leq |V|$ .  $\square$

**Running example (continued).** For LXV-B2:  $N = 5$ ,  $|V| = 2$ . Under the general bound (Theorem 4):  $D(w) \leq 2 \times 4 = 8$ . Under the adjacent-swap regime of Theorem 5, which the chamber enforces via  $\text{max\_rank\_shift} \leq 1$ :  $D(w) \leq |V| = 2$ . The chamber’s operational budget  $k_{\text{allowed}} = 1$  is thus conservative relative to the tighter bound of 2.

**Theorem 6** (Degeneracy Index Bounds the Maximum Inversion Budget). *Fix baseline window  $w_0 = 1$  and let the baseline magnitudes be ordered  $S_1(i_1) \geq \dots \geq S_1(i_N)$  with adjacent gaps  $\Delta_k$ . Assume a uniform perturbation envelope  $\sigma_P$  such that  $|S_w(s) - S_1(s)| \leq \sigma_P$  for all  $s \in \mathcal{N}$ ,  $w \in W$ .*

Define the vulnerable-gap set  $V = \{k : \Delta_k \leq 2\sigma_P\}$  and Degeneracy Index  $\mathcal{D} = |V|/(N-1)$ . Assume the adjacent-swap regime  $\max_s |r_w(s) - r_1(s)| \leq 1$ . Then for every  $w \in W$ ,

$$D(w) \leq |V| = (N-1)\mathcal{D}.$$

Consequently, any inversion-budget rule  $D(w) \leq k_{\text{allowed}}$  is guaranteed achievable under the adjacent-swap regime provided  $k_{\text{allowed}} \geq (N-1)\mathcal{D}$ . In particular, choosing  $k_{\text{allowed}} := |V|$  is a principled conservative upper budget. The minimal necessary budget in the adjacent-swap regime is  $k_{\text{allowed}}^{\min} = \nu(V)$  (Theorem 7).

*Proof.* Fix  $w \in W$ . Under the adjacent-swap regime, every inversion is a swap of two items adjacent in the baseline order, crossing exactly one boundary  $k$ . At a crossing of boundary  $k$ :  $S_1(i_k) \geq S_1(i_{k+1})$  but  $S_w(i_k) < S_w(i_{k+1})$ . Applying the envelope twice,

$$\Delta_k = S_1(i_k) - S_1(i_{k+1}) \leq (S_1(i_k) - S_w(i_k)) + (S_w(i_{k+1}) - S_1(i_{k+1})) \leq 2\sigma_P,$$

hence  $k \in V$ . Moreover, since no station moves more than one rank, no single boundary  $k$  can be crossed by more than one independent inversion: doing so would require a rank shift of magnitude  $\geq 2$ . Therefore distinct inversions correspond to distinct elements of  $V$ , giving  $D(w) \leq |V| = (N-1)\mathcal{D}$ . The budget implications are immediate.  $\square$

**Corollary 1** (Principled  $k_{\text{allowed}}$  Choice for LXV-B2). *In LXV-B2, the gate  $\max_s |r_w(s) - r_1(s)| \leq 1$  is enforced. Therefore it is principled to set*

$$k_{\text{allowed}} := |V|,$$

where  $V = \{k : \Delta_k \leq 2\sigma_P\}$  is computed from baseline gaps and the smoothing envelope. The chamber's choice of  $k_{\text{allowed}} = 1$  is conservative relative to the theoretically derived budget  $|V| = 2$ .

**Definition 9** (Matching Number of Vulnerable Gaps). *Given envelope  $\sigma_P$  and vulnerable set  $V = \{k \in \{1, \dots, N-1\} : \Delta_k \leq 2\sigma_P\}$ , a subset  $M \subseteq V$  is disjoint if it contains no two adjacent indices:*

$$k \in M \implies (k-1) \notin M \text{ and } (k+1) \notin M.$$

The matching number is

$$\nu(V) := \max\{|M| : M \subseteq V \text{ is disjoint}\}.$$

Note that  $\nu(V) \leq |V|$ , with equality if and only if  $V$  contains no two adjacent indices.

**Remark 4** (One-line computation of  $\nu(V)$  on a path). *Sort  $V$  in increasing order and scan left-to-right; greedily pick index  $k$  whenever  $k > \text{lastPicked} + 1$  (initialise  $\text{lastPicked} = -\infty$ ). The count of picked indices equals  $\nu(V)$ . This is the standard maximum matching on a path graph, solvable in  $O(|V|)$  time.*

**Theorem 7** (Minimal Necessary Inversion Budget – Adjacent-Swap Regime). *Assume the uniform envelope  $|S_w(s) - S_1(s)| \leq \sigma_P$  for all  $s \in \mathcal{N}$ ,  $w \in W$ , and the adjacent-swap regime  $\max_s |r_w(s) - r_1(s)| \leq 1$ .*

*Then for every  $w \in W$ :*

$$D(w) \leq \nu(V).$$

*Moreover the bound is tight: there exists a perturbation satisfying both the envelope and the adjacent-swap regime for which  $D(w) = \nu(V)$ .*

*Consequently, the minimal certification budget that is guaranteed not to false-fail any admissible perturbation is*

$$k_{\text{allowed}}^{\min} = \nu(V).$$

*Proof sketch. (Upper bound.)* Under  $\max_s |r_w(s) - r_1(s)| \leq 1$ , the permutation from  $R_1$  to  $R_w$  is a product of *disjoint* adjacent transpositions: no element participates in two swaps, so crossed boundaries form a disjoint subset of  $\{1, \dots, N - 1\}$ . The envelope argument shows each crossed boundary  $k$  must satisfy  $\Delta_k \leq 2\sigma_P$ , hence lie in  $V$ . Therefore the crossed boundaries form a disjoint subset of  $V$ , and  $D(w) \leq \nu(V)$ .

*(Tightness.)* Let  $M \subseteq V$  be a maximum disjoint subset,  $|M| = \nu(V)$ . For each  $k \in M$ , set  $S_w(i_k) = S_1(i_k) - \sigma_P$  and  $S_w(i_{k+1}) = S_1(i_{k+1}) + \sigma_P$ . Since boundaries in  $M$  are disjoint, no element is perturbed twice; the rank shift of every element is at most 1, preserving the adjacent-swap regime. Each boundary  $k \in M$  satisfies  $\Delta_k \leq 2\sigma_P$ , so  $S_w(i_k) < S_w(i_{k+1})$ , realising one inversion per boundary. Thus  $D(w) = \nu(V)$ .

*(Minimality.)* The tightness construction is an admissible instance, so any rule with  $k_{\text{allowed}} < \nu(V)$  would false-fail it. Hence  $k_{\text{allowed}}^{\min} = \nu(V)$ .  $\square$

**Corollary 2** (When  $|V|$  is minimal). *If  $V$  contains no two adjacent indices (all vulnerable gaps are separated), then  $\nu(V) = |V|$  and the minimal necessary budget equals  $|V|$ .*

**Remark 5** (LXV-B2 – El Mayor instantiation). *El Mayor B2 has two vulnerable tail gaps at positions  $k = 3$  and  $k = 4$  (gaps of 0.484 mm and 0.499 mm respectively), which are adjacent indices. Therefore  $|V| = 2$  but  $\nu(V) = 1$ : only one of the two boundaries can be swapped without forcing*

any element to shift two ranks. The minimal necessary inversion budget is  $k_{\text{allowed}}^{\min} = \nu(V) = 1$ , which equals the chamber's operational choice exactly. The chamber's gate is therefore not merely conservative – it is the tight minimal budget derived from the perturbation envelope and the adjacent-swap constraint.

## 7 Inversion Distance and Rank Correlation

**Lemma 2** (Kendall  $\tau$  is determined by inversion count). *Let  $R_1$  and  $R_w$  be two total orders on  $N$  items with inversion count  $D(w)$ . Then Kendall's  $\tau$  satisfies*

$$\tau(w) = 1 - \frac{4D(w)}{N(N-1)}.$$

**Corollary 3** (Theorem-grade  $\tau$  lower bounds from vulnerability). *Under the assumptions of Theorem 4, for every  $w \in W$ :*

$$\tau(w) \geq 1 - \frac{4}{N(N-1)} \sum_{k \in V} (N-k) \geq 1 - \frac{4|V|}{N}.$$

*If moreover the adjacent-swap regime of Theorem 5 holds, then*

$$\tau(w) \geq 1 - \frac{4|V|}{N(N-1)}.$$

**Definition 10** (Adjacent-swap benchmark model for Spearman  $\rho$ ). *Fix  $N$  and integer  $k \geq 0$ . The benchmark model takes  $R_w$  to be obtained from  $R_1$  by performing exactly  $k$  disjoint adjacent swaps (each swap exchanges positions  $j$  and  $j+1$  for some  $j$ , with all swapped pairs disjoint). Let  $\rho_{\text{bench}}(N, k)$  denote Spearman's  $\rho$  between  $R_1$  and  $R_w$  under this model.*

**Lemma 3** (Spearman benchmark value under  $k$  disjoint adjacent swaps). *Under the benchmark model of Definition 10,*

$$\rho_{\text{bench}}(N, k) = 1 - \frac{12k}{N(N^2-1)}.$$

**Remark 6** (Status of  $\rho$  in this paper). *Unlike Kendall  $\tau$ , Spearman  $\rho$  is not determined solely by inversion count: different patterns of inversions yield different values of  $\sum d_i^2$ . Accordingly,  $\rho_{\text{bench}}$  is used in this paper as a reporting benchmark calibrated to the adjacent-swap interpretation (one tolerates at most  $k = |V|$  such swaps), not as a theorem-grade lower bound valid for all perturbation patterns.*

**Running example (LXV-B2,  $N = 5$ ).** The certification gate enforces  $D(w) \leq k_{\text{allowed}} = 1$ . If a window yields exactly one inversion ( $D(w) = 1$ ), then by Lemma 2,

$$\tau(w) = 1 - \frac{4}{5 \cdot 4} = 0.80.$$

Under the adjacent-swap benchmark model,

$$\rho_{\text{bench}}(5, 1) = 1 - \frac{12}{5(25 - 1)} = 0.90.$$

These match the reported minima in LXV-B2 (`kendall_min: 0.8, spearman_min: 0.9`). Kendall  $\tau$  is fully determined by  $D$ , while Spearman  $\rho$  is reported relative to the adjacent-swap benchmark.

## 8 Topology Stability

Let  $\theta_w(i)$  denote displacement azimuth at station  $i$  under window  $w$ . Let  $C_w$  be the clustering assignment under directional  $k$ -means.

**Definition 11** (Angular Separation and Drift). *Let  $\Theta$  denote the centroid separation between clusters (computed at baseline  $w_0$ ). The angular drift  $\delta_P$  induced by smoothing is bounded by the displacement perturbation normalised by the minimum baseline magnitude:*

$$\delta_P \leq \frac{\sigma_P^{(\text{emp})}}{\min_s S_1(s)}.$$

*This bound follows because the azimuth of a vector  $\mathbf{v}$  changes by at most  $\sin^{-1}(\delta/\|\mathbf{v}\|)$  under a perturbation of size  $\delta$ ; for small  $\delta/\|\mathbf{v}\|$  this is bounded above by  $\delta/\|\mathbf{v}\|$ .*

**Theorem 8** (Topology Rigidity). *If*

$$\Theta > 2\delta_P,$$

*then cluster assignment is invariant across all admissible windows:*

$$\text{ARI}(C_w, C_{w'}) = 1 \quad \forall w, w'.$$

**Remark 7** (TOPO\_SINGLE edge case). *For events classified as TOPO\_SINGLE (a single displacement cluster, e.g. Ridgecrest LXV-C2 with `sep = 0`), the centroid separation  $\Theta$  is undefined because there is no second centroid. In this case  $\text{ARI} = 1$  holds trivially and is not a validation of Theorem 8; it is a degenerate case the theorem does not cover. A single-cluster event provides no discriminating evidence for or against the topology framework.*

## 9 Perturbation Geometry and Directional Stability

### 9.1 Vector Representation of Station Displacements

For each station  $s \in \mathcal{N}$ , let the co-seismic displacement vector be

$$\mathbf{u}_w(s) = (d_E(s, w), d_N(s, w)) \in \mathbb{R}^2.$$

Define the baseline configuration  $\mathbf{u}_1(s) := \mathbf{u}_{w_0}(s)$  with  $w_0 = 1$ , and let  $\|\mathbf{u}\| := \sqrt{d_E^2 + d_N^2}$  denote Euclidean magnitude. We interpret smoothing as a perturbation operator

$$\mathbf{u}_w(s) = \mathbf{u}_1(s) + \boldsymbol{\varepsilon}_w(s),$$

with bounded perturbation envelope  $\|\boldsymbol{\varepsilon}_w(s)\| \leq \sigma_P$  (Admissibility condition 1 ensures the envelope is uniform across stations and windows).

**Remark 8** (Consistency with scalar envelope). *The scalar perturbation used in Section 3 is  $|S_w(s) - S_1(s)| = \left| \|\mathbf{u}_w(s)\| - \|\mathbf{u}_1(s)\| \right| \leq \|\boldsymbol{\varepsilon}_w(s)\| \leq \sigma_P$  by the reverse triangle inequality. The vector envelope thus implies the scalar envelope used in all rank-stability theorems.*

### 9.2 Angular Perturbation Envelope

Let  $\theta_w(s) := \arg(\mathbf{u}_w(s))$  denote the displacement azimuth under window  $w$ . Define the angular perturbation bound

$$\delta_P := \sup_{s \in \mathcal{N}, w \in W} |\theta_w(s) - \theta_1(s)|.$$

**Lemma 4** (Angular Drift Bound). *If  $\|\boldsymbol{\varepsilon}_w(s)\| \leq \sigma_P$  and  $\|\mathbf{u}_1(s)\| \geq m > 0$ , then*

$$|\theta_w(s) - \theta_1(s)| \leq \arcsin\left(\frac{\sigma_P}{m}\right).$$

*In particular,*

$$\delta_P \leq \arcsin\left(\frac{\sigma_P}{\min_s \|\mathbf{u}_1(s)\|}\right) \leq \frac{\sigma_P}{\min_s \|\mathbf{u}_1(s)\|}$$

*for small  $\sigma_P / \min_s \|\mathbf{u}_1(s)\|$ .*

*Proof.* The maximal angular deviation of  $\mathbf{u}_w = \mathbf{u}_1 + \boldsymbol{\varepsilon}$  relative to  $\mathbf{u}_1$  is achieved when  $\boldsymbol{\varepsilon}$  is orthogonal to  $\mathbf{u}_1$ . In that configuration,

$$\sin |\theta_w - \theta_1| = \frac{\|\boldsymbol{\varepsilon}\|}{\|\mathbf{u}_1\|} \leq \frac{\sigma_P}{\|\mathbf{u}_1(s)\|}.$$

Taking the supremum over  $s$  and  $w$  and applying arcsin completes the proof.  $\square$

**Remark 9** (Consistency with the  $\delta_P$  bound in Section 8). *Lemma 4 provides the rigorous derivation of the bound  $\delta_P \leq \sigma_P / \min_s S_1(s)$  stated in Section 8. The two are consistent:  $S_1(s) = \|\mathbf{u}_1(s)\|$  by definition.*

### 9.3 Directional Cluster Separation

Let the baseline directional configuration partition the stations into  $K$  clusters  $\mathcal{C}_1, \dots, \mathcal{C}_K$  under directional  $k$ -means, with minimal inter-cluster angular separation

$$\Theta_{\min} = \min_{i \neq j} \inf_{s \in \mathcal{C}_i, t \in \mathcal{C}_j} |\theta_1(s) - \theta_1(t)|.$$

**Theorem 9** (Directional Stability Theorem). *If  $\Theta_{\min} > 2\delta_P$ , then for all  $w \in W$  the cluster assignment is invariant:*

$$\mathcal{C}_i(w) = \mathcal{C}_i(1) \quad \forall i.$$

*Proof.* For any  $s \in \mathcal{C}_i$  and  $t \in \mathcal{C}_j$  with  $i \neq j$ ,

$$|\theta_w(s) - \theta_w(t)| \geq |\theta_1(s) - \theta_1(t)| - |\theta_w(s) - \theta_1(s)| - |\theta_w(t) - \theta_1(t)| \geq \Theta_{\min} - 2\delta_P > 0.$$

Hence  $s$  and  $t$  cannot exchange angular order under any admissible window, so no station can migrate between clusters.  $\square$

**Remark 10** (Relationship to Theorem 8). *Theorem 9 is the vector-geometric version of the Topology Rigidity Theorem (Theorem 8). The earlier theorem stated the result with  $\Theta$  and  $\delta_P$  as given quantities; Lemma 4 now grounds  $\delta_P$  in the perturbation envelope  $\sigma_P$  and the minimum baseline magnitude, making both theorems jointly computable from the same noise estimate  $\hat{\sigma}$ .*

### 9.4 Geometric Rigidity Modulus

**Definition 12** (Geometric Rigidity Modulus).

$$\mathcal{R}_{\text{geo}} := \frac{\Theta_{\min}}{2\delta_P}.$$

By Theorem 9:  $\mathcal{R}_{\text{geo}} > 1$  implies directional rigidity;  $\mathcal{R}_{\text{geo}} \leq 1$  permits directional degeneration.

## 9.5 Unified Structural Stability Condition

Recall the magnitude rigidity modulus  $\mathcal{R}_{\text{mag}} := \min_k \Delta_k / (2\sigma_P)$  (Definition 6). Define the *unified rigidity vector*

$$\mathcal{R} := (\mathcal{R}_{\text{mag}}, \mathcal{R}_{\text{geo}}).$$

**Corollary 4** (Unified Phase Classification). *Under perturbation-admissible smoothing:*

1. If  $\mathcal{R}_{\text{mag}} > 1$  and  $\mathcal{R}_{\text{geo}} > 1$ , the system is fully rigid: both rank order and directional cluster assignment are invariant across all  $w \in W$ .
2. If either component equals 1, the system lies on the corresponding phase boundary.
3. If  $\mathcal{R}_{\text{mag}} \leq 1$ , rank inversion is admissible (bounded by  $\nu(V)$  under the adjacent-swap regime). If  $\mathcal{R}_{\text{geo}} \leq 1$ , directional degeneration is admissible.

Both components share the same noise-derived  $\sigma_P$  (via Theorems 1 and 2 for magnitude; Lemma 4 for angle), so the full stability state  $\mathcal{R}$  is computable from a single noise estimate  $\hat{\sigma}$ .

**LXV suite instantiation.** For LXV-A (Kumamoto):  $\mathcal{R}_{\text{mag}} \approx 21.6$ ,  $\mathcal{R}_{\text{geo}} \gg 1$  (cosines  $\approx 0.996$  across all windows). For LXV-B2 (El Mayor):  $\mathcal{R}_{\text{mag}} \approx 0.19$ ,  $\mathcal{R}_{\text{geo}} \gg 1$  (direction cosines  $> 0.9999$ ). For LXV-C2 (Ridgecrest):  $\mathcal{R}_{\text{mag,eff}} \approx 4.7$ ,  $\mathcal{R}_{\text{geo}}$  undefined (TOPO\_SINGLE, Remark 7). El Mayor is therefore the paradigmatic case of a system with degenerate *magnitude* rigidity but robust *directional* rigidity – the two components of  $\mathcal{R}$  can and do decouple in real data.

## 10 RNP Integration as a Phase-Boundary Theorem

### 10.1 Rigid and Nonrigid Descriptions as a Quotient Constraint

Let  $X$  denote the rigid realization space of admissible encodings for an event  $E$ : full time series, detrending choices, smoothing window choice, and other admissible interface degrees of freedom.

Let  $G_{\text{adm}}$  denote the groupoid generated by admissible interface transforms, including variation over  $w \in W$  and admissibility gates that preserve the LXV protocol.

Let  $\Pi : X \rightarrow Y$  denote the induced projection from rigid realizations to the nonrigid structural signature space  $Y$ , where a signature consists of the magnitude-order structure  $R_w$ , inversion statistics  $D(w)$  and  $\nu(V)$ , directional partition  $C_w$ , and topology invariants (ARI stability, separation scores).

The Rigid–Nonrigid Transition Principle (RNP) requires that any law-like observable must *descend* to the quotient by admissible transforms: it must be constant on  $G_{\text{adm}}$ -orbits and factor through  $\Pi$ .

## 10.2 Phase Coordinates

The phase coordinate vector is

$$\mathcal{R} = (\mathcal{R}_{\text{mag}}, \mathcal{R}_{\text{geo}})$$

with components as defined in Sections 3 and 9.

**Definition 13** (Rigid Phase).  *$E$  is in the rigid phase if  $\mathcal{R}_{\text{mag}} > 1$  and  $\mathcal{R}_{\text{geo}} > 1$ .*

**Definition 14** (Boundary Degeneracy Phase).  *$E$  is in the boundary degeneracy phase if either modulus lies in  $(0, 1]$  while admissibility constraints remain satisfied and degeneracy is bounded.*

**Definition 15** (Nonrigid / Fragmentation Phase).  *$E$  is in the nonrigid phase if either modulus drops sufficiently below 1 that rank order or directional partition is not invariant across admissible transforms.*

## 10.3 RNP Phase-Boundary Theorem

**Theorem 10** (RNP Phase-Boundary Theorem). *Assume the perturbation-admissible family  $W$  and the adjacent-swap regime  $\max_s |r_w(s) - r_1(s)| \leq 1$ .*

1. **(Rigid descent)** *If  $\mathcal{R} > (1, 1)$  componentwise, then the structural signature*

$$\Sigma(E) := (R_w, D(w), \nu(V), C_w)_{w \in W}$$

*is invariant on each  $G_{\text{adm}}$ -orbit; equivalently,  $\Sigma$  descends through the quotient and is law-admissible.*

2. **(Boundary forcing)** *If  $\mathcal{R}$  meets a phase boundary ( $\mathcal{R}_{\text{mag}} \leq 1$  or  $\mathcal{R}_{\text{geo}} \leq 1$ ), then any attempt to enforce a single rigid description fails to descend: there exist admissible transforms under which the rigid description changes, and bounded degeneracy is structurally forced.*

3. (**Nonrigid impossibility**) *If either modulus is sufficiently small that no bounded-degeneracy certificate holds (inversion budget cannot be bounded by  $\nu(V)$ , or  $\Theta_{\min} \leq 2\delta_P$ ), then no orbit-invariant structural signature exists in the restricted model class and fragmentation is unavoidable.*

*Proof outline.* (1) Suppose  $\mathcal{R}_{\text{mag}} > 1$  but rank order is not invariant. Then some adjacent gap inverts under an admissible perturbation, requiring  $\Delta_k \leq 2\sigma_P$  – contradicting  $\min_k \Delta_k > 2\sigma_P$ . Suppose  $\mathcal{R}_{\text{geo}} > 1$  but directional partition is not invariant. Then  $\Theta_{\min} \leq 2\delta_P$  – contradiction. In the interior rigid region both structures are invariant across  $W$ , hence descend.

(2) If  $\mathcal{R}_{\text{mag}} \leq 1$  there exists  $k \in V$ . Under the adjacent-swap regime there exist admissible realizations that swap across a disjoint vulnerable boundary, changing  $R_w$  and breaking descent. The directional case is analogous.

(3) If neither rank nor directional structure can be bounded-invariant, any candidate signature changes along the orbit and no law-admissible invariant exists in the class.  $\square$

## 10.4 Empirical Instantiation (LXV Phase Placement)

The LXV suite provides empirical instances of all required logical branches: rigid descent (LXV-A Kumamoto, LXV-C2 Ridgecrest:  $D(w) = 0$  and  $\text{ARI} = 1$  across all  $w$ ); boundary forcing (LXV-B2 El Mayor:  $\nu(V) = 1$ , observed  $D(w) = 1$  under adjacent-swap regime, topology remaining rigid); no observed full fragmentation within the tested admissible family.

Thus co-seismic displacement hierarchies instantiate a measurable RNP phase boundary in a displacement field setting.

# 11 Embedding in the UNNS Substrate

## 11.1 Admissible Operators and Nested Resolution

Within the UNNS Substrate framework, each smoothing window  $w \in W$  is interpreted as an admissible operator

$$\mathcal{O}_w : X \rightarrow X$$

acting on the nested representation of the seismic event. The family  $\{\mathcal{O}_w\}_{w \in W}$  forms a partially ordered admissible operator set under resolution refinement: larger  $w$  corresponds to coarser resolution and greater averaging of substrate dynamics.

The perturbation envelope

$$\|\mathbf{u}_w(s) - \mathbf{u}_1(s)\| \leq \sigma_P$$

is therefore not arbitrary noise. It is a bounded admissible deformation inside the operator grammar of the substrate:  $\sigma_P$  measures how far any admissible operator can move the displacement vector from its baseline realization.

## 11.2 Structural Identifications

The correspondence between perturbation-stability constructs and UNNS substrate objects is as follows.

Perturbation-stability construct	UNNS substrate object
Smoothing window $w \in W$	Admissible operator $\mathcal{O}_w$
Perturbation envelope $\sigma_P$	Bounded admissible deformation radius
Rigidity modulus $\mathcal{R}$	Admissibility margin in substrate phase space
Degeneracy index $\mathcal{D}$	Boundary proximity measure
Descent of $\Sigma$ through $\Pi$	Quotient stability (law-admissibility)
Phase boundary $\mathcal{R} = 1$	RNP-critical surface in the substrate

This correspondence shows that the phase structure proven in Theorem 10 is not a standalone robustness result but an admissibility-geometry statement inside the UNNS substrate.

## 11.3 Admissibility Margin

**Definition 16** (Admissibility Margin).

$$\mathcal{A} := \min(\mathcal{R}_{\text{mag}}, \mathcal{R}_{\text{geo}}).$$

The admissibility margin has a direct substrate interpretation:

- $\mathcal{A} > 1$ : the structural signature is invariant across admissible operators; the signature descends in the substrate.
- $\mathcal{A} = 1$ : the system lies on the admissibility boundary; rigid descriptions are unstable under arbitrarily small operator deformations.
- $\mathcal{A} < 1$ : multiple non-equivalent structural realizations coexist under admissible transforms; descent fails.

**Proposition 1** (Admissible Operator Descent Criterion). *Let  $\{\mathcal{O}_w\}_{w \in W}$  be the admissible operator family in the UNNS Substrate, with perturbation envelope  $\|\mathbf{u}_w - \mathbf{u}_1\| \leq \sigma_P$  and admissibility margin  $\mathcal{A} = \min(\mathcal{R}_{\text{mag}}, \mathcal{R}_{\text{geo}})$ .*

*If  $\mathcal{A} > 1$ , then for every admissible operator composition  $\mathcal{O}_{w_1} \circ \dots \circ \mathcal{O}_{w_k}$  with  $w_i \in W$ , the induced structural signature  $\Sigma = (R_w, D(w), \nu(V), C_w)$  is invariant.*

*If  $\mathcal{A} \leq 1$ , there exists an admissible operator within the nesting family under which  $\Sigma$  changes.*

*Proof.* The first claim follows directly from the RNP Phase-Boundary Theorem (Theorem 10, part 1):  $\mathcal{A} > 1$  implies both  $\mathcal{R}_{\text{mag}} > 1$  and  $\mathcal{R}_{\text{geo}} > 1$ , so by Theorems 1 and 9 the rank order and directional partition are invariant across all  $w \in W$ , hence across any composition of admissible operators. The matching number  $\nu(V) = 0$  when  $\mathcal{R}_{\text{mag}} > 1$  (no vulnerable gaps), so  $D(w) = 0$  is preserved. The second claim follows from part 2 of Theorem 10: when  $\mathcal{A} \leq 1$  at least one modulus meets its boundary, and the tightness construction of Theorem 7 provides a specific admissible operator realization that changes  $\Sigma$ .  $\square$

## 11.4 Substrate Interpretation of the Phase Boundary

The RNP Phase-Boundary Theorem (Theorem 10) is therefore an admissibility-geometry theorem:

Structural lawhood in the UNNS Substrate exists precisely in the interior of admissibility margin  $\mathcal{A} > 1$ . Boundary degeneracy corresponds to admissibility-critical configurations; the non-rigid regime corresponds to substrate phase fragmentation under admissible operator nesting.

**LXV admissibility margins.** Kumamoto (LXV-A):  $\mathcal{A} = \min(21.6, \gg 1) \gg 1$  (deep substrate interior). El Mayor (LXV-B2):  $\mathcal{A} = \min(0.19, \gg 1) = 0.19$  (substrate boundary, magnitude channel only). Ridgecrest (LXV-C2):  $\mathcal{A}_{\text{eff}} = \min(4.7, N/A) = 4.7$  (single-cluster topology; magnitude channel rigid).

The decoupling of  $\mathcal{R}_{\text{mag}}$  and  $\mathcal{R}_{\text{geo}}$  in El Mayor demonstrates that the two admissible operator channels – resolution refinement of magnitudes and resolution refinement of directions – can reach their respective phase boundaries at different substrate configurations.

## 12 Empirical Estimation of the Rigidity Modulus (LXV Suite)

### Operational Definitions

- Baseline window:  $w_0 = 1$ .
- Empirical perturbation amplitude  $\sigma_P^{(\text{emp})}$ : maximal absolute deviation  $\max_{s,w} |S_w(s) - S_1(s)|$  over valid stations and  $w > 1$ .
- Adjacent gaps  $\Delta_k$ : computed from descending baseline magnitudes.
- Only stations with valid  $\text{SNR}_h \geq 5$  are used.

#### 12.1 LXV-A / Kumamoto 2016 (Rigid Phase)

Baseline magnitudes (mm): 787.94, 453.88, 324.07, 51.44.  
 Adjacent gaps: 334.06, 129.81, 272.63.  
 min  $\Delta_k = 129.81$  mm;  $\sigma_P^{(\text{emp})} \approx 3.0$  mm.

$$\mathcal{R} = \frac{129.81}{2 \times 3.0} \approx 21.6 \gg 1.$$

No inversions observed. Spearman = 1, Kendall = 1. Consistent with rigid phase; Theorem 1 applies.

#### 12.2 LXV-C2 / Ridgecrest 2019 (Rigid Phase)

Baseline magnitudes (mm): 679.17, 235.12, 226.22, 169.41, 44.78, 32.94.

Adjacent gaps: 444.05, 8.90, 56.81, 124.63, 11.84.

Global minimum:  $\Delta_{\min} = 8.90$  mm (ranks 2 and 3).  $\sigma_P^{(\text{emp})} \approx 6.1$  mm;  $2\sigma_P \approx 12.2$  mm.

The global modulus  $\mathcal{R}_{\text{global}} = 8.90/(2 \times 6.1) \approx 0.73$  places this event formally in the boundary regime. However,  $\sigma_P$  is dominated by station P595 (a near-fault station with  $\sim 679$  mm displacement whose window-to-window variation is large in absolute terms). The pair-specific perturbation relevant to the rank-2/rank-3 boundary – stations CCCC and P580 – is far smaller, placing the effective modulus for that pair well above 1. Using the smallest *effective* vulnerable gap (56.81 mm, ranks 3–4):

$$\mathcal{R}_{\text{effective}} \approx \frac{56.81}{2 \times 6.1} \approx 4.7 > 1.$$

No inversion observed. This confirms the prediction and motivates pair-specific Rigidity Moduli (see Section 13).

### Topology: LXV-C2 (Ridgecrest)

Ridgecrest is classified `TOPO_SINGLE` with cluster separation `sep = 0`. As noted in Remark 7, this is a degenerate case; the perfect ARI does not constitute a topology theorem test.

### 12.3 LXV-B2 / El Mayor 2010 (Boundary Phase)

Baseline magnitudes (mm): 104.94, 49.11, 7.95, 7.46, 6.96.

Adjacent gaps: 55.83, 41.16, 0.484, 0.499.

$\min \Delta_k = 0.484$  mm;  $\sigma_P^{(\text{emp})} \approx 1.3$  mm.

$$\mathcal{R} = \frac{0.484}{2 \times 1.3} \approx 0.19 \ll 1.$$

Observed: one inversion in selected windows, max rank shift = 1, Spearman  $\geq 0.9$ , Kendall  $\geq 0.8$ . Consistent with boundary degeneracy; Theorem 5 predicts  $D(w) \leq 8$ ; observed maximum is 1.

### 12.4 LXV-D / El Mayor Topology (Rigid Phase)

Angular centroid separation:  $\Theta \approx 69^\circ$ .  $\delta_P < 1.5^\circ \ll \Theta/2$ . Topology is rigid (ARI = 1 across all windows) as predicted.

### Summary of Empirical $\mathcal{R}$ and Phase Classification

Event	$\min \Delta_k$ (mm)	$\sigma_P$ (mm)	$\mathcal{R}$	Phase
Kumamoto (A)	$\sim 130$	$\sim 3$	$\sim 21.6$	Rigid
Ridgecrest (C2)	$\sim 57\text{--}125$ (eff.)	$\sim 6$	4.7–10	Rigid
El Mayor (B2)	0.484	$\sim 1.3$	$\sim 0.19$	Boundary

### Discriminative power of $\mathcal{R}$

The three events span two orders of magnitude in  $\mathcal{R}$  (0.19, 4.7, 21.6) despite comparable moment magnitudes ( $M_w \approx 7$ ). This stratification is not a function of event size but of near-fault geometry: El Mayor’s five stations cluster tightly in displacement space (sub-millimetre gaps between the three smallest magnitudes), while Kumamoto’s four stations are well-separated across three distance zones from the fault. The  $\mathcal{R}$  metric therefore encodes station network geometry and proximity distribution, not just seismic energy release, making it a discriminating structural diagnostic beyond what magnitude alone provides.

## 13 Falsifiability

The framework admits the following distinct falsification classes.

### Falsifiers of the Theorem (structure is wrong):

1.  $D(w) > 0$  while  $\mathcal{R} > 1$  under the empirical envelope. This falsifies Theorem 1 and implies the perturbation bound was violated – either the noise model is inadequate or  $\sigma_P$  is underestimated.
2. Cluster reassignment ( $\text{ARI} < 1$ ) while  $\Theta > 2\delta_P$ . This falsifies Theorem 8.
3. Inversion count exceeding the Degeneracy Bound  $|V|(N - 1)$ . This would falsify Theorem 5.

### Falsifiers of the parameter estimates (model fit is wrong):

4. An observed inversion while  $\widehat{\mathcal{R}}(\alpha) > 1$  for the chosen  $\alpha$ . This does not falsify the theorem (it may be a rare  $\alpha$ -probability event) but does falsify the sub-Gaussian noise model assumptions or the guard-day protocol.
5. Systematic monotone dependence of  $\widehat{\mathcal{R}}(\alpha)$  on  $w$  inconsistent with the  $\sigma/\sqrt{w}$  decay prediction. This would indicate violated independence assumptions across epochs.
6.  $D(w)$  systematically exceeding  $|V|$  in the boundary regime despite adjacent-only perturbations. This would falsify the tighter k-allowed bound argued in Section 6.

### Degenerate non-evidence:

7. Perfect ARI in a `TOPO_SINGLE` event provides no evidence for or against Theorem 8 (see Remark 7).
8. The Ridgecrest global  $\mathcal{R}_{\text{global}} = 0.73 < 1$  combined with no observed inversion is consistent with the theory (boundary regime is not a guarantee of inversion) and does not constitute an anomaly.

## Discussion

**Pair-specific Rigidity Modulus.** The global  $\sigma_P$  is dominated by the station with the highest displacement variation (P595 in Ridgecrest). A pair-specific modulus

$$\mathcal{R}^{(i,j)} := \frac{\Delta_{ij}}{\sigma_P^{(i,j)}}, \quad \sigma_P^{(i,j)} = \max_w |S_w(i) - S_w(j) - [S_1(i) - S_1(j)]|,$$

provides a tighter per-pair bound:  $\sigma_P^{(i,j)} \leq 2\sigma_P$  but is often much smaller. For Ridgecrest, the global  $\mathcal{R}_{\text{global}} = 0.73$  is misleading because the relevant rank-2/rank-3 pair has a much larger pair-specific modulus, explaining the empirically observed stability.

**Guard days and design tradeoff.** Guard days  $g$  reduce the usable epoch count  $m$ , which increases  $\sigma_P(\alpha)$  and decreases  $\widehat{\mathcal{R}}(\alpha)$ . This is an explicit design tradeoff: excluding post-seismic contamination comes at the cost of a smaller theoretical stability margin. An optimal guard-day choice  $g^* = \arg \max_g \widehat{\mathcal{R}}(g, \alpha)$  is event-dependent.

## Conclusion

Perturbation-admissible smoothing preserves structural order and topology whenever magnitude and angular separation exceed the perturbation envelopes  $2\sigma_P$  and  $2\delta_P$  respectively. The Rigidity Modulus provides a single scalar that localises each event on the rigid–boundary–fragmentation spectrum. The LXV suite instantiates this spectrum empirically: Kumamoto ( $\mathcal{R} \approx 21.6$ ) sits deep in the rigid phase, El Mayor B2 ( $\mathcal{R} \approx 0.19$ ) demonstrates bounded boundary degeneracy, and Ridgecrest ( $\mathcal{R}_{\text{eff}} \approx 4.7$ ) is rigid after accounting for station geometry. The two-order-of-magnitude spread in  $\mathcal{R}$  across events of comparable magnitude demonstrates the framework’s power as a structural diagnostic beyond seismic energy alone.

## A Empirical Phase Structure and Degeneracy Index (LXV Suite)

This appendix provides numerical instantiation of the Rigidity Modulus and Degeneracy Index for each LXV event.

### A.1 LXV-A: Kumamoto 2016

$\min \Delta_k = 129.81$  mm;  $\sigma_P \approx 3.0$  mm;  $2\sigma_P = 6$  mm. All gaps  $\gg 6$  mm;  $|V| = 0$ ;  $\mathcal{D} = 0$ ;  $\mathcal{R} \approx 21.6$ . Observed: no inversions. Fully rigid phase.

### A.2 LXV-C2: Ridgecrest 2019

$\sigma_P \approx 6.1$  mm;  $2\sigma_P \approx 12.2$  mm. Only the 8.90 mm gap satisfies  $\Delta_k \leq 12.2$  mm;  $|V| = 1$ ;  $\mathcal{D} = 1/5 = 0.2$ ;  $\mathcal{R}_{\text{global}} \approx 0.73$ . Observed: no inversions.  $\mathcal{D}$  predicts vulnerability, not necessity.

### A.3 LXV-B2: El Mayor 2010

$\min \Delta_k = 0.484$  mm;  $\sigma_P \approx 1.3$  mm;  $2\sigma_P \approx 2.6$  mm. Both tail gaps (0.484 and 0.499 mm) satisfy  $\Delta_k \leq 2.6$  mm;  $|V| = 2$ ;  $\mathcal{D} = 2/4 = 0.5$ ;  $\mathcal{R} \approx 0.19$ . Observed: one inversion; max rank shift = 1. Boundary degeneracy.

### A.4 Empirical Phase Summary

Event	$\mathcal{R}$	$\mathcal{D}$	Observed Regime
Kumamoto	$\gg 1$	0	Rigid
Ridgecrest	$> 1$ (effective)	0.2	Rigid
El Mayor (B2)	$\ll 1$	0.5	Boundary

The Degeneracy Index predicts the fraction of adjacent pairs vulnerable to inversion; the Rigidity Modulus determines phase classification.